

SYNTHESIS OF NONLINEAR ALGORITHMS FOR MULTIMODE CONTROL OF TRANSPORT ENTERPRISES IN AN INDETERMINATE STATE

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Abstract

Modern living conditions and growing uncertainties in the decision in choosing strategy conduct for transport enterprises, define the trend to create automatic systems of decision-making and forecasting. The fundamental and powerful argument for the creation of fuzzy logic systems is the reduction of costs (resource consumption) now as a result of economic and technological activities. Rational use of resources now depends on the basic performance management system. The proposed methods of information processing in the existing algorithms cannot solve this problem in its entirety, so synthesis proposed new algorithms and approaches that are used to build neural networks, with the possibility of learning.

In this article we consider the problem of synthesis of nonlinear algorithms for multi-mode process control (transport company) in the state space. A new algorithmic approach to the synthesis of the non-linear multi-mode controller for TP (transport companies), the disclosure of which is given in the form of a set of linear models is presented. At the executive management level to ensure solved the problem of maintaining high-precision settings to (dynamically changing object) with given constraints on the dynamic characteristics of the system. For example, TP, these restrictions are related to ensuring high reliability of functioning of the ACS (automatic control system). Design decisions at the executive level of the synthesis process control algorithms are implemented on the basis of algorithms that satisfy the principle of minimal complexity.

A characteristic feature of the search task of project solutions at the executive level is the need to take account of the nonlinear nature of the work of TP in different modes of operation, which significantly complicates the problem of defining the optimal solution.

Keywords: transport companies, control systems, fuzzy logic, neural networks, control algorithms.

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1. Introduction

Consider the features of the information model of executive-level automation systems (information transport enterprise management system), which reflect the characteristics of the information flows at the executive level of the TA. The generalized information model can be simplified, taking into account the assumption that changes depending on the TP parameters on environmental parameters.

2. Materials and Methods

In [1–3] it is stated that the method of decentralized management is widely spread in the management of multidimensional nonlinear objects. Thus ACS is divided into a number of individual (autonomous) subsystems, each of which performs a particular measurement position controlled. Compare it with the setpoint (command) and the production of the control action, coming on to the appropriate input.

3. Experimental procedures

In the classical formulation of the control synthesis problem in the state space for a linear system it is assumed that given the controlled linear system with constant coefficients

$$\dot{x} = Ax + bu, \quad (1)$$

$$\dot{x} = Ax + bk^T x = (A + bk^T)x, \quad (2)$$

the roots of the characteristic equation $\det[A + bk^T - \lambda E] = 0$, appeared equal to specified numbers $\{\lambda\}$.

If you use linear transducers for the linear system of differential equations $\dot{x} = My$, $M = (m_1, \dots, m_n)$, (m_i – eigenvector), the solution will have the form

$$x = M(\exp \text{diag}(\lambda) M^{-1} x_0 = (\exp At) x_0. \quad (3)$$

For non-linear systems of the form

$$\dot{x} = X(x) = A(x)x. \quad (4)$$

By analogy with the linear systems we can write the equation for the eigenvalues and eigenvectors as follows:

$$A(x)m_s(x) = \lambda(x)m_s(x), \quad s = 1 + n. \quad (5)$$

Substitute non-linear transformation $x = M(x)y$, where $M(x) = (m_1(x), m_2(x), \dots, m_n(x))$ in (5) we get

$$\dot{M}(x)y + M(x)\dot{y} = A(x)M(x)y, \quad (6)$$

From (6) we find a solution in the form

$$\dot{y} = \dot{M}^{-1}(x)M(x)\dot{y} = A(x)M^{-1}(x)y. \quad (7)$$

Because the term $\dot{M}^{-1}(x)M(x)\dot{y}$ in (7) impermissible judgment about the stability of the system (4) only the roots of the characteristic equation

$$\det(A(x) - \lambda(x)E) = 0, \quad (8)$$

as in equation (7) the matrix $\dot{M}^{-1}(x)M(x)\dot{y} \neq 0$.

If $\lambda_r = \lambda_s(x)$ for $A(x)$, but $m_s = \text{const}, s = 1 + n$, those. matrix $M(x)$ It is made up of permanent and vectors $M(x) = 0$, then the solution of the system (4) can be represented as follows:

$$x = x_0 \exp \int_t^t A(x) d\tau.$$

3. 1. Synthesis of nonlinear ACS TP specified point-linear models

In the first stage of the conditions specified accuracy approximation TP characteristics formed the set of linear dynamic models; describe the dynamic properties of the TA for small deviations of controlled origin in the vicinity of N modes. Each (i-I) Linear Model TP is as follows:

$$\dot{x} = A_i x + B_i u,$$

$$y = C_i x + D_i u.$$

$$(\mathbf{B}_i \mathbf{B}_i^+ - \mathbf{E})(\mathbf{M}_\lambda \text{diag}(\lambda)_i - \mathbf{A}_i \mathbf{M}_{\pi\lambda}) = 0, \quad (9)$$

3. 2. The entropy of the environment

$$H(F) = - \int_{U(F)} p(F) \ln p(F) dF. \quad (11)$$

Let the nonlinear ACS TP is be described as follows

$$\dot{x} / dt = Ax + H(x) + Bu(x), \quad (12)$$

Consider the search task management solution $u(x)$. Set up a system of equations for the eigenvectors and eigenvalues of the linear and nonlinear parts of the system (12) based on control and condition (12)

$$\begin{aligned}\lambda_s \mathbf{m}_s &= (\mathbf{A} + \mathbf{B} \mathbf{k}^T) \mathbf{m}, \\ \rho_s \mathbf{m}_s &= \mathbf{H}(\mathbf{m}_s) + \mathbf{B} \mathbf{U}(\mathbf{m}_s).\end{aligned}\tag{13}$$

$$\begin{aligned} \lambda m_1 &= a_{11}m_1 + + a_{1n}m_n + b_1k_1m_1 + + b_1k_nm_n, \\ \\ \lambda m_1 &= a_{n1}m_n + + a_{nn}m_n + b_nk_1m_1 + + b_nk_nm_n. \end{aligned} \tag{14}$$
$$B(\lambda, k)_m = 0, \quad (15)$$
$$P = \det(B(\lambda, k)) = C_n(k)\lambda^n + C_{n-1}(k)\lambda^{n-1} + \dots + C_0(k) = 0. \quad (16)$$
$$\begin{aligned}\lambda_{\text{s}}\text{m}_{\text{s}1} &= -2\text{m}_{\text{s}1} + \text{m}_{\text{s}2} + \text{k}_1\text{m}_{\text{s}1} + \text{k}_2\text{m}_2; \\ \lambda_{\text{s}}\text{m}_{\text{s}1} &= -\text{m}_{\text{s}2} + 2\text{k}_1\text{m}_{\text{s}1} + 2\text{k}_2\text{m}_2; \\ \text{p}_{\text{s}}\text{m}_{\text{s}1} &= \text{m}_{\text{s}2}^2; \\ \text{p}_{\text{s}}\text{m}_{\text{s}2} &= -\text{m}_{\text{s}1}^2,\end{aligned}\tag{17}$$
$$\begin{aligned} f_1 &= (\lambda_s + 2 - k_1)m_{s_1} + (-1 - k_2)m_{s_2} = 0; \\ f_2 &= -2k_1m_{s_1} + (\lambda_s - 1 - k_2)m_{s_2} = 0; \\ f_3 &= m_{s_1}^2 + m_{s_2}^3 = 0. \end{aligned}$$

$$\begin{aligned} a_1 &= \lambda_s + 2 - k_1, a_2 = -1 - k_2; \\ a_3 &= -2k_1, a_7 = \lambda_c - 1 - 2k_7. \end{aligned} \quad (18)$$
$$\begin{aligned} S_p(f_1, f_3) &= m_{s1}^2 f_1 - a_1 f_3 = a_2 m_{s1}^2 - a_1 m_{s2}^2 = f_4 = 0; \\ S_p(f_2, f_4) &= a_2 m_{s1} f_2 - a_3 f_4 = a_2 a_4 m_{s1} - a_1 a_2 a_3 = f_5 = 0; \\ S_p(f_2, f_5) &= a_2 a_1 f_2 - a_3 f_5 = m_{s2} (a_2 a_4^2 - a_1 a_2^3) = f_6 = 0. \end{aligned} \quad (19)$$
$$f_6 = f(\lambda_c, k) = 0. \quad (20)$$
$$S(\lambda, k) = -(1 - k_y)(\lambda - 1 - 2k_y)^2 + (\lambda + 1 - k_y)4k_y^2 = 0. \quad (21)$$
$$k_1/2 - k_2 = -5/3.$$

4. Results

[illegible]
$$\begin{aligned} \dot{x} &= A_i(x - x_i^{cm}) + B_i(u - u_i^{cm}), \\ y &= y_i^{cm} + C_i(x - x_i^{cm}) + D_i(u - u_i^{cm}), \end{aligned} \quad (23)$$

6. Conclusions

2. A method of synthesis of nonlinear ACS TP defined piecewise linear models, using constant eigenvectors, allowing to provide the desired quality of regulation in the partial pickup modes. This

approach allows the use of different approaches to the synthesis of linear regulators with the additional condition of constancy of the matrix of the canonical basis of a closed system.

3. The criterion of control for nonlinear systems with homogeneous right-hand sides.

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